

Pointing and Amplitude Calibration Concepts

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Outline



- Beams & Pointing
- Antenna Efficiency, Antenna Temperature
- SEFD as the key for calibration
- System Temperature & Gain
- rxg & antabfs files

Why Calibrate?



- Scientific quality:
 - geodesy best SNR per scan to improve delay precision
 - astronomy source brightness on absolute physical scale
 - \circ Regular checks of calibration \rightarrow help notice problems

You can measure/calibrate:

- the focus & pointing
- the aperture efficiency (η_A)
- \circ the system temperature (T_{sys})
- the gain curve

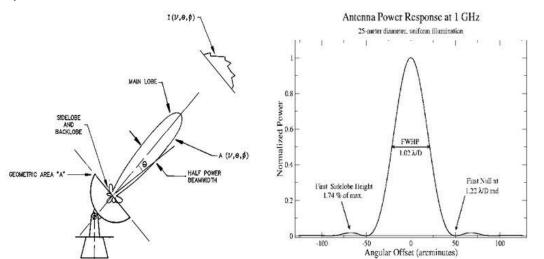
• Related maintenance workshops:

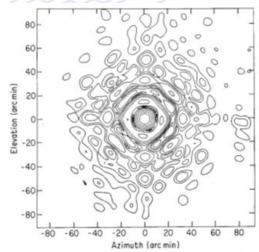
- Antenna Gain Calibration (Lindqvist)
- Field System Operations (Neidhardt)
- Automated Pointing Models Using the FS (Himwich) [TOWs ≤ 2019]

Antenna Beam-width



- Directivity: power received (or transmitted) should form a small (solid) angle. Roughly $\theta = \lambda / D$
 - 14 GHz on 12m antenna \rightarrow ~ 6.1'
- Half-power beam-width (HPBW): angle from beam axis such that power falls to one-half of the maximum.





Antenna Pointing Issues



- Ideally, radio source centered in main beam
- Pointing error 10% HPBW causes 3% loss of sensitivity

20% HPBW

10%

30% HPBW

22%

- Detailed analysis of pointing errors required to achieve a pointing model good to 10% HPBW across entire sky:
 - alignment errors, encoder offsets, antenna deformation
 - ► "Automated Pointing Models" workshop from previous TOWs
- Radial feed offset will significantly reduce the gain
 - The feed should be $< \lambda/4$ from the radial focal point
 - The focal length may change with elevation
 - \circ Lateral offest $< \lambda$ mostly biases pointing, with less loss of gain

Antenna Efficiency



Power received from an unpolarized source by a perfect antenna:

$$P = \frac{1}{2} S A_{geom} \Delta v$$

- \circ Units of S = Jansky (10⁻²⁶ Watts per m² per Hz)
- Effective aperture: fraction of total power actually picked up by real antenna: $A_{eff} = \eta_A A_{geom}$
- η_A is the aperture efficiency. It depends on:
 - Reflector surface accuracy
 - Feed illumination / spill-over
 - Subreflector / leg blockage
- η_{Δ} can be a function of pointing direction

Antenna Temperature



A resistive load at temperature T delivers a power of:

$$P = k T \Delta v$$

- $k = \text{Boltzmann constant } (1.308 \times 10^{-23} \text{ Joules per Kelvin})$
- Antenna Temperature: T of a resistive load providing the same power as a source in the antenna beam:

$$T_A = 1/(2k) \eta_A A_{geom} S$$
$$= \pi D^2/(8k) \eta_A S$$

Larger, more efficient antennas & brighter sources yield higher T_A

System Temperature (T_{svs})



• T_{sys} is the temperature of a resistive load providing the same power as the system noise:

$$T_{sys} = T_{rcvr} + T_{struct} + T_{sky}$$

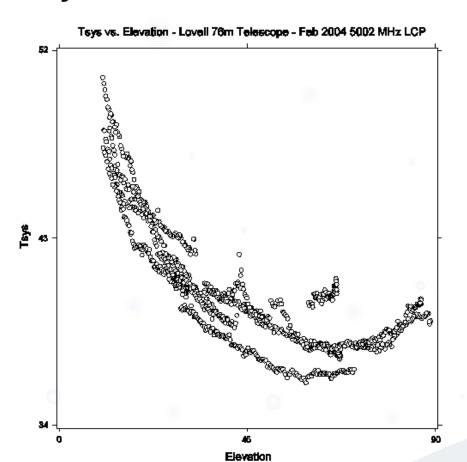
- o rcvr: LNAs, mixers, etc.
- o struct: antenna structure, ground spill-over, sidelobes, etc.
- o sky: atmospheric path-length, cosmic backgrounds, RFI, etc.

$$T_{atm} = T_{zenith} (1 - e^{-\tau/\sin(El)})$$

- \bullet T_{svs} itself can have an elevation dependence
- Note: T_{sys} is almost always \rightarrow T_A

T_{sys} vs. elevation





$$T_{atm} = T_{zenith} (1 - e^{-\tau/sin(El)})$$

System Equivalent Flux Density



- SEFD = flux-density of a fictitious source delivering the same power as the system noise.
- Direct relation between T_{sys} & SEFD:

$$T_{sys}[K] = \Gamma[K/Jy] \cdot SEFD[Jy]$$

- Gain (or sensitivity) Γ gives the increase in the Γ of the equivalent resistive load for a source of 1 Jy.
 - \circ Thus in a sense the ratio of $T_{sys} & T_A$ sets the sensitivity
- Going back a couple viewgraphs:

$$\Gamma = \eta_A \pi D^2 / (8k)$$

$$\approx 3x 10^{-4} \eta_A D^2$$

Importance of SEFD



- Invariably in radio astronomy, system noise dominates over power from the source in the beam.
 - Nominal X-band SEFDs in [Jy] (see, e.g., EVN status table):
 Ef=20, Ys=200, Mc=320, Nt=840, On=785, Tm65=48
- In this case, geometric means of SEFD's at the two stations in a baseline

 → conversion scale between correlation coefficient and physical amplitude
 in Jy.
- With $SEFD = T_{SVS}/\Gamma$, there are 2 parts to calibrate:
 - System temperature
 - o Gain

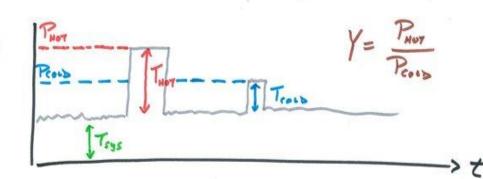
Y-method for finding T_{sys}



Put loads at 2 different temperatures "into" antenna:

$$P_{hot} = g (T_{hot} + T_{sys})$$

$$P_{cold} = g (T_{cold} + T_{sys})$$



• Form ratio of P_{hot} / P_{cold} (= Y) & solve this for T_{sys} :

$$T_{\rm sys} = \frac{T_{\rm hot} - Y T_{\rm cold}}{Y - 1}$$

Assumptions: receiver remains in linear regime; g, T_{sys} constant

T_{sys} via a cal-diode at T_{cal}

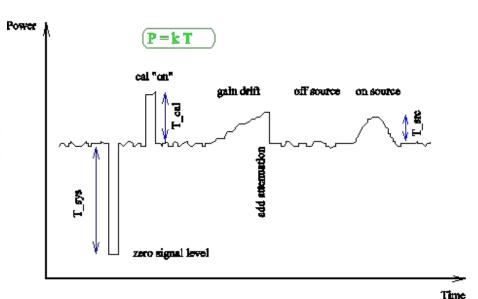


Noise-cal signal at T_{cal}:

$$P_{on} = g (T_{cal} + T_{sys})$$
 $P_{off} = g (T_{sys})$

$$\frac{P_{off}}{P_{on} - P_{off}} = \frac{gT_{sys}}{g(T_{cal} - T_{sys}) - gT_{sys}}$$

$$= \frac{T_{sys}}{T_{cal}}$$
 $T_{sys} = T_{cal} \frac{P_{off}}{P_{on} - P_{off}}$



- \bullet T_{sys} needs an accurate measurement of T_{cal}
- Sources for T_{svs} calib.: strong, non-variable, point-like

T_{cal} via hot & cold loads



• A measure of T_{cal} can also come from hot & cold loads:

$$P_{cal.on} - P_{cal.off} = g (T_{cal} + T_{sys}) - g (T_{sys}) = g (T_{cal})$$

$$P_{hot} - P_{cold} = g (T_{hot} - T_{cold})$$

Forming ratios & solving for T_{cal} gives:

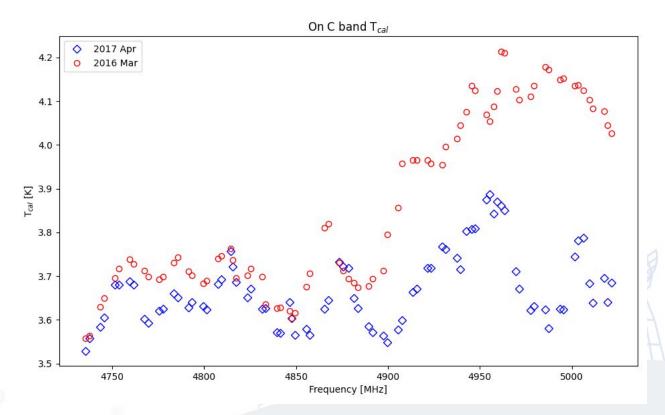
$$T_{\rm cal} = (T_{\rm hot} - T_{\rm cold}) \frac{P_{\rm cal.on} - P_{\rm cal.off}}{P_{\rm hot} - P_{\rm cold}}$$

 \bullet T_{cal} can be a function of time (session to session) and frequency (even within a single IF-sized range)

T_{cal} variations

JIVE
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Onsala85 at 6cm



► "Amplitude Gain Calibration" Workshop (Lindqvist)

Gain parameterization



- We've seen $T_{svs} = \Gamma \cdot SEFD$
- We can solve this for SEFD:

$$SEFD = \frac{T_{\text{sys}}}{GAIN} = \frac{T_{\text{sys}}}{DPFU \times g(z)}$$

- DPFU (degrees per flux unit) is an absolute gain
- g(z) is the gain curve as a function of zenith angle (or elevation,...),
 typically expressed as a polynomial

$$g(z) = c_0 + c_1 z + c_2 z^2 + \ldots + c_n z^n$$

o g(z) stems mainly from gravitational deformations to the antenna structure (\rightarrow aparabolic, focal-length changes, etc.)

Gain Determination



 The gain can be determined from the powers on & off source and the powers with the cal-diode on & off:

$$P_{cal.on} - P_{cal.off} = g (T_{cal} + T_{sys}) - g T_{sys} = g T_{cal}$$

$$P_{on.src} - P_{off.src} = g (T_A + T_{sys}) - g T_{sys} = g T_A$$

• Forming the ratio gives: T_{cal}/T_A , where T_A can further be written as GAIN·S (S = source flux density)

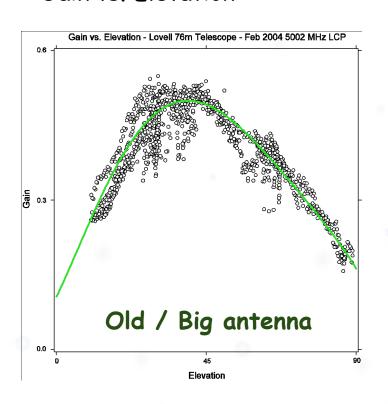
$$GAIN = \frac{P_{\text{on.src}} - P_{\text{off.src}}}{P_{\text{cal.on}} - P_{\text{cal.off}}} \frac{T_{\text{cal}}}{S}$$

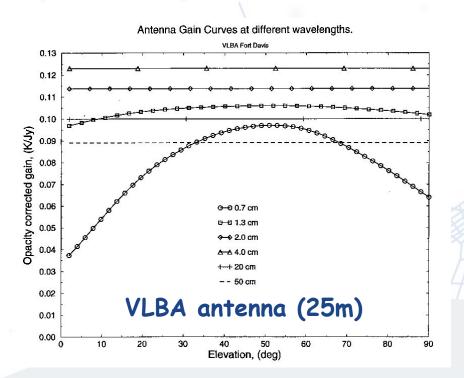
FS program aquir to collect gain-calibration data

Gain Curve



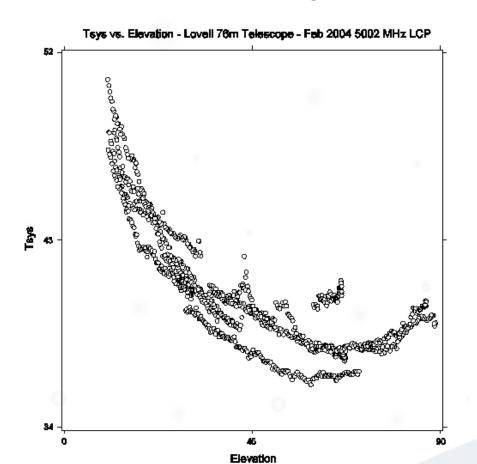
• Gain vs. Elevation:





Reminder of T_{sys} vs. elevation





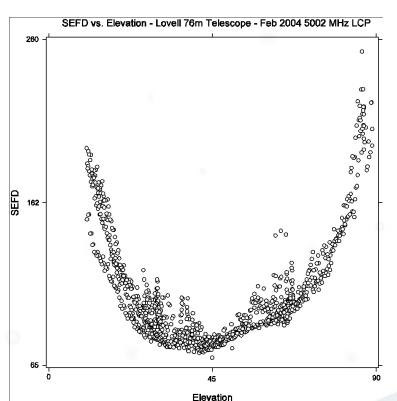
$$T_{atm} = T_{zenith} (1 - e^{-\tau/\sin(El)})$$

SEFD example for Lovell



SEFD vs. elevation:

$$SEFD = T_{sys}/GAIN$$



Summary (of "theory")



 Combination of DPFU, gain curve, and T_{cal} required to provide accurate calibration (SEFD)

- \circ $\mathsf{T}_{\mathsf{cal}} \to \mathsf{T}_{\mathsf{sys}}$
- \circ DPFU, gain curve \rightarrow GAIN
- \circ SEFD = $T_{sys} / GAIN$
- Other workshops detail their determination:
 - "Automated Pointing Models Using the FS" from previous TOWs
 - "Antenna Gain Calibration" (Lindqvist)
- T_{cal} vs. frequency: determine this regularly
- Gain curve: measure at least once per year

FS Power Measurements



- caltemp: broad-band noise source at a specific T
- Total power integrators:
 - o tpi: measured when cal-source is off
 - tpical: measured when cal-source is on
 - o tpzero: zero levels
- Cal-source "fires" only when not recording
 - o tpi': a tpi value measured close in time to a cal-source firing
 - tpdiff: (tpical tpi') essentially sets the scale between TPI
 counts and the physical temperature
 - \circ "not recording" \rightarrow long-enough gaps in schedule (>10s)

T_{sys} from FS TPIs



Output with the cal-source on & off:

$$g\left(T_{cal} + T_{sys}\right) =$$
tpical - tpzero $g\left(T_{sys}\right) =$ tpi - tpzero

• Forming the ratio & solving for T_{sys} gives:

$$T_{\rm sys} = T_{\rm cal} \frac{\text{tpi-tpzero}}{\text{tpical-tpi'}}$$

- Representative tpical tpi' value ~ 1000
 - \circ Too low \rightarrow larger scatter
 - \circ ~ 0 \rightarrow dead cal-source (?)
 - Jumps → change in attenuation; unstable cal-source

What the Astronomer Wants



- \bullet T_{sys} within an experiment
 - o tpical tpi': provides a tie to the T_{cal} at gaps
 - o tpi: provides a relative T scale between gaps
- SEFD: noise (in flux-density units) of telescopes

$$SEFD(t) = \frac{T_{\rm sys}(t)}{GAIN} = \frac{T_{\rm sys}(t)}{DPFU \times POLY(elev)}$$

- DPFU: an absolute sensitivity (gain) parameter [K/Jy]
- POLY: the gain curve
- ullet Dimensionless correlation coefficients o physical flux densities via the geometric mean of the SEFD's of the two stations forming a baseline

Continuous Calibration



- FS supports two calibration schemes for DBBCs
 - o [1] Non-continuous: as described so far...
 - [2] Continuous: cal-source switched on/off at 80Hz
- [1]: only tpi monitored during recording by tpicd

```
2024.291.12:00:00.14#tpicd#tpcont/11,6129,5925,1u,6175,5774,21,5977,5574,2u,5987,5580,ia,3145.38 2024.291.12:00:00.14#tpicd#tpcont/91,6282,5970,9u,6045,5777,al,6173,5984,au,6057,5805,ic,3008.89 2024.291.12:00:00.28#tpicd#tpcont/11,6129,5925,1u,6175,5774,21,5977,5574,2u,5987,5580,ia,3245.94 2024.291.12:00:00.28#tpicd#tpcont/91,6282,5970,9u,6045,5777,al,6173,5984,au,6057,5805,ic,2979.93
```

• [2]: tpicd monitors both tpi and tpi' continuously

```
2024.291.12:00:15.37#tpicd#tpi/11,12922,1u,12114,21,11929,2u,12385,ia,953.98
2024.291.12:00:15.37#tpicd#tpi/91,12529,9u,12144,al,11761,au,11897,ib,922.73
2024.291.12:00:30.39#tpicd#tpi/11,14093,1u,12187,21,11896,2u,12387,ia,1004.17
2024.291.12:00:30.39#tpicd#tpi/91,12557,9u,12102,al,11754,au,11892,ib,933.84
2024.291.12:00:45.39#tpicd#tpi/11,13666,1u,12108,21,11909,2u,12384,ia,963.25
2024.291.12:00:45.39#tpicd#tpi/91,14702,9u,12143,al,11729,au,11894,ib,1013.62
```

No tpi/, tpical/, or tpdiff/ lines in continuous-cal logs

Continuous Cal: Advantages



- Less affected by time-variations in gain
- More straightforward scheduling (astronomy)
 - Cal-source "firing" occurs in preob last ~10s of gap
 - End of gap defined from the "global" scan start time
 - Cal-source "firing" best done while antenna on-source
 - Slower antennas may not yet be on-source at scan start (→ non-zero data_good field in the vex-file)
 - Some PIs have made individual-station schedules in order to delay cal-source "firing" for the slower stations, via the essentially "local" scan start-times in each 1-station schedule

rxg Files

- 9 "lines"
 - 1) Applicable frequency range
 - 2) Creation date
 - 3) Beam width
 - 4) Available polarizations
 - 5) DPFU for each pol.
 - 6) Gain curve
 - 7) Pol. / Freq. / T_{cal} data
 - 8) Receiver temp / opacity
 - 9) Spill-over noise T

```
* first line: LO values and ranges, format:
     type frequencies [MHz]
* if type is range, the two values: lower and upper frequencies
* if type is fixed, then one or two fixed value
* 2nd line: creation date
* format: yyyy ddd or yyyy mm dd (0 is valid for all for intial set-up)
2010 02 02
 3rd line: FWHM beamwidthm format:
 if type is frequncy, then fwhm=value*1.05*c/(freq*diameter)
                       value is 1.0 if omitted
* if type is constant, then fwhm=value (degrees)
frequency 1.0
* 4th line polarizations available
* 5th line: DPFU (degrees/Jansky) for polarizations in previous line in order
0.094500 0.09450000
* 6th line: gain curve (only one) for ALL polarizations in 4th line
 TYPE FORM COEFFICENTS ...
                             [max coeffs = 10]
     FORM = POLY only for now
     TYPE - ELEV only for now
     COEFFICENTS - variable number of number values
ELEV POLY 8.69503E-01 2.33055E-03 -1.05562E-05
 7th and following lines: tcal versus frequency
      Format: POL FREQ TCAL
                 polarization rcp or lcp
                 frequency [MHz]
                 [K]
      MAXIMUM ENTRIES 800, group by polarization, then by increasing freq
1cp 1607.0 15.4945
1cp 1609.0 16.3480
1cp 1611.0 17.5200
1cp 1613.0 18.6960
1cp 1615.0 20.0320
rcp 1607.0 22.6755
rcp 1609.0 22.6380
rcp 1611.0 23.0090
rcp 1613.0 23.3990
rcp 1615.0 23.8450
end_tcal_table
* Trec - receiver temperature, degrees K
* if value is zero, no opacity corrections are used
 Spillover table
      format: elevation temperature
   elevation is angular degrees above horizon
  temperature is Kelvin degrees of spillover noise
*spillover table ends with end_spillover_table record
end spillover table
```

The antabfs Program



- Reads FS logs and rxg files in order to:
 - Compute (tpical tpi') or tpcont values for each VC/BBC
 - \circ Compute/edit the resulting T_{svs} values
 - o Output an .antabfs file (for use in AIPS, CASA)
- Originally in perl (C. Reynolds, J. Yang, J. Quick)
- Shifts to python (Yebes: F. Beltrán, J. González)
 - Fuller DBBC support (e.g., also now form=wastro)
 - Continuous-cal support
 - Obwnload antabfs.py from github: https://github.com/evn-vlbi/VLBI-utilities

antabfs (output) file



- "GAIN"
 - Gain curve, DPFU,
 Frequency Range
- INDEX line
- T_{sys} (t, sideband)

```
! Amplitude calibration data for JB in n2413.
! For use with AIPS task ANTAB.
! Waveband(s) = 13.2cm.
! RXG files used for each LO:
   Setup 01
     L0=2272.00 MHz lcp calJb2272.rxg 2021 11 18
     L0=2272.00 MHz rcp calJb2272.rxg 2021 11 18
! DBBC used in mode DDC
! Produced on 2024-10-24 using antabfs.py version: 2019-10-11
GAIN JB ELEV DPFU=1.15,1.15 FREQ=1578.49,1738.49
POLY=0.780400926175,0.0121277693428,-0.000212881052904,1.15149509363e-06 /
TSYS JB FT = 1.0 TIMEOFF=0
INDEX= 'R1', 'R2', 'R3', 'R4', 'L1', 'L2', 'L3', 'L4'
! Setup 01
! Calibration mode: CONT
!Column 1 = R1: ifA, bbc01, 1610.49 MHz , LSB, BW= 32.00 MHz, Tcal=17.75 K
!Column 2 = R2: ifA, bbc01, 1642.49 MHz , USB, BW= 32.00 MHz, Tcal=17.36 K
!Column 3 = R3: ifA, bbc02, 1674.49 MHz , LSB, BW= 32.00 MHz, Tcal=20.67 K
!Column 4 = R4: ifA, bbc02, 1706.49 MHz , USB, BW= 32.00 MHz, Tcal=15.97 K
!Column 5 = L1: ifB, bbc09, 1610.49 MHz , LSB, BW= 32.00 MHz, Tcal=14.70 K
!Column 6 = L2: ifB, bbc09, 1642.49 MHz , USB, BW= 32.00 MHz, Tcal=15.59 K
!Column 7 = L3: ifB, bbc10, 1674.49 MHz , LSB, BW= 32.00 MHz, Tcal=20.77 K
!Column 8 = L4: ifB, bbc10, 1706.49 MHz , USB, BW= 32.00 MHz, Tcal=14.47 K
! 291 11:38.87: scanNum=0001 scanName=no0001 source=3c395
291 12:00.09 77.4 78.9 101.9 59.8 64.3 66.9 109.2 58.6
291 12:00.17 74.7 78.4 190.9 51.3 63.8 70.3 108.2 58.6
291 12:00.25 76.7 76.8 101.9 60.0 64.2 67.7 110.5 58.5
291 12:00.34 75.9 77.3 102.0 59.7 63.7 70.9 108.7 58.6
291 12:00.42 75.1 81.9 102.1 59.7 63.5 68.2 108.7 58.6
291 12:00.50 75.4 81.1 103.6 59.8 64.0 68.6 117.2 58.6
```



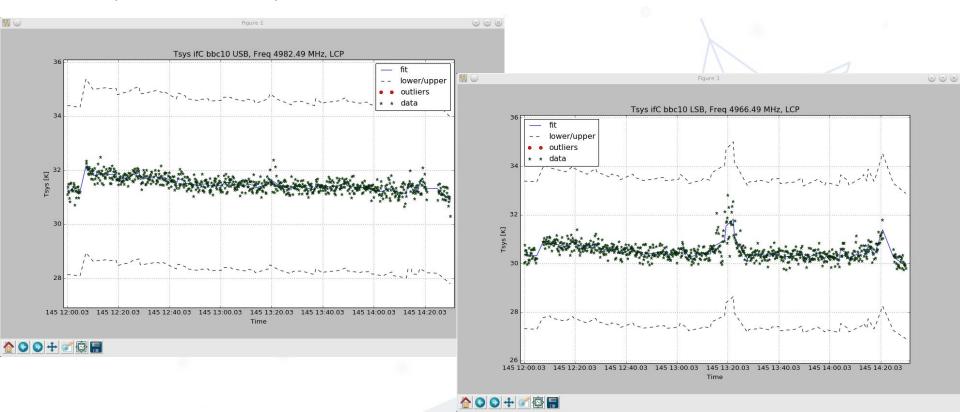
Running antabfs.py



- Syntax:
 - antabfs.py [-f rxg_files_list] fs_log_file
 - Looks for rxg file in /usr2/control/rxg_files/ (self.rxgDirectory)
 - -f: optionally specify the rxg file explicitly (correct freq.band?)
- Antabfs.py will cycle through the sidebands
 - \circ Opens a plot window showing the derived T_{sys} + fit + bounds
 - "Outlier" points appear in red
 - \circ Interactively edit out T_{sys} points via making drag+click boxes
 - When happy with this sideband, close the plot window
- A final all-sideband plot appears (not editable)
- Closing this window \rightarrow query to save into an antabfs file

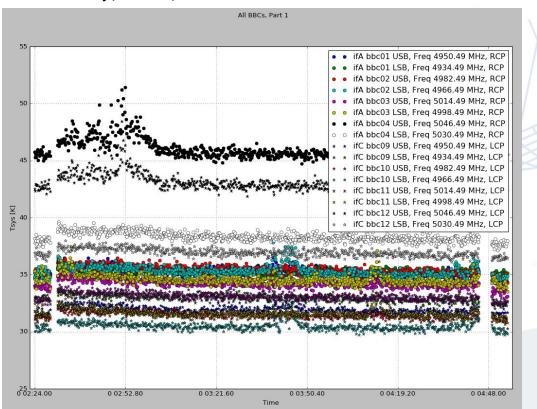
antabfs.py: sideband plots





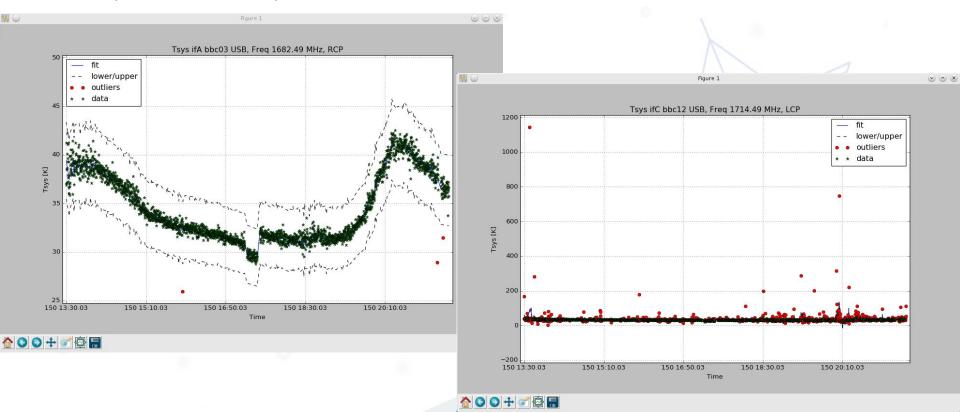
antabfs.py: final plots



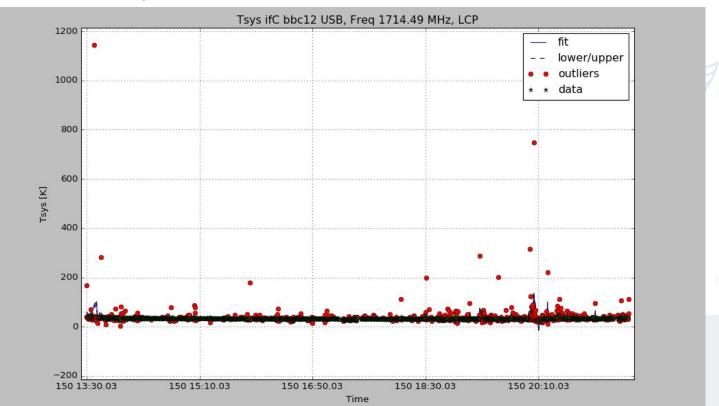


antabfs.py: case needing edits

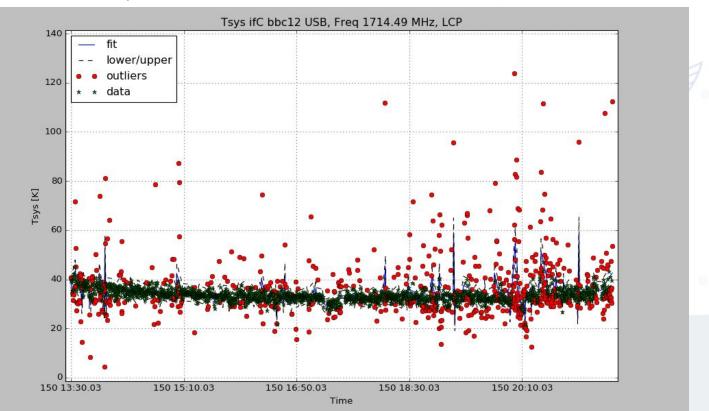




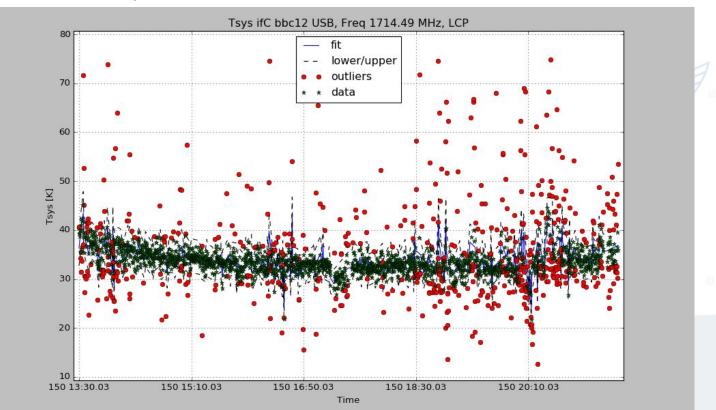






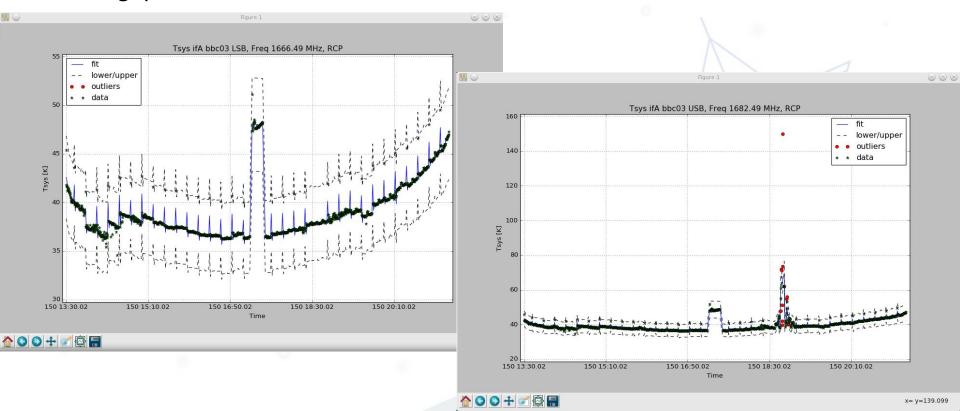




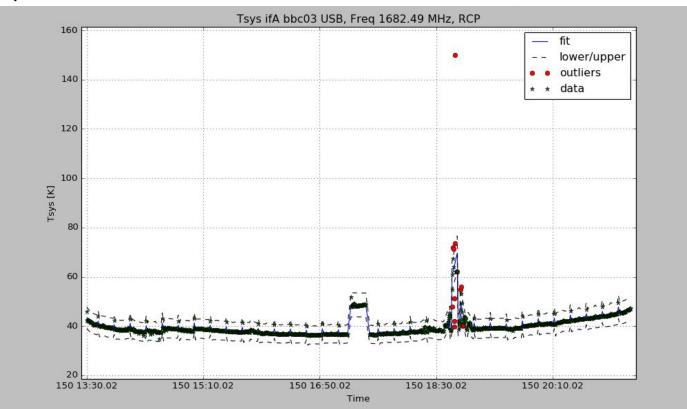


antabfs.py: not continuous cal.

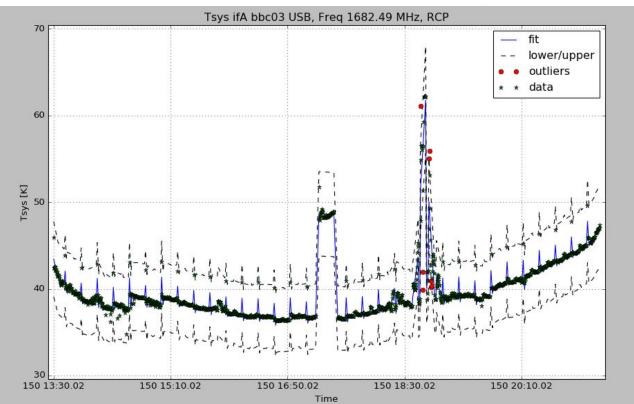






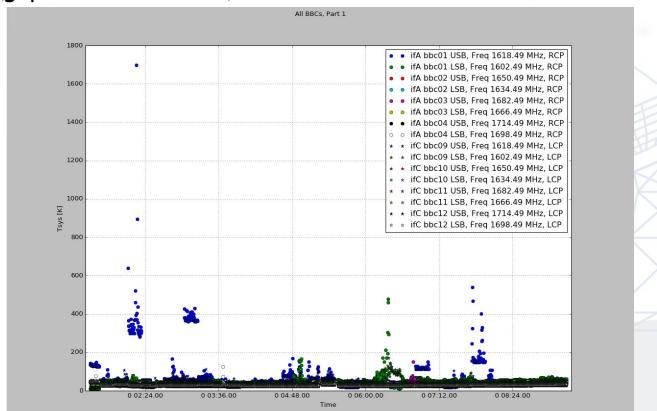






antabfs.py: t-, v-localized RFI





Summary (of "antabfs")



- Quality of stations' antabfs file has direct bearing on quality of resulting imaging
 - Keep rxg files up-to-date!
- Provide antabfs files in timely fashion
 - They serve as input into pipelining & user analysis
- Stations in a better position to run antabfs.py than are the correlators (local knowledge)
- Feedback about antabfs.py → Yebes or JIVE
 - Javier González (jgonzalez@oan.es)
 - Fran Beltrán (franciso.beltran@oan.es)